



Radiation exposure from five different concrete mixtures

Measurement of activity
concentrations, radon
exhalation and dose
assessment

Confidential

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Summary

As part of the here presented work a total of five different concrete mixtures have been studied to determine the activity concentrations and the radon exhalation as well as an assessment of the radiation exposure when these concrete mixtures are used in regular dwellings. Experiments are carried out in compliance with the Dutch standards NEN 5697 and NEN 5699.

Based on these experimental findings, a dose assessment for both external and internal radiation exposure is performed. The results indicate an estimated external dose between 0.20 and 0.26 mSv per year and an internal dose between 0.55 and 0.62 mSv per year. Based on those estimates the maximum total dose for these concrete mixtures is about 0.85 mSv.

Introduction

As part of the here presented work a total of five different concrete mixtures have been studied to determine the activity concentrations and the radon exhalation as well as an assessment of the radiological dose when these materials are used in regular dwellings.

An analysis has been carried out on the radioactivity concentrations of gamma-ray emitting radionuclides in three samples for each of the five concrete mixtures, according to the Dutch standard NEN 5697. For the determination of the ^{222}Rn exhalation rate a test is carried out for each concrete mixture according to the Dutch standard NEN 5699.

Subsequently, a dose assessment for both internal and external radiation exposure is performed for these five concrete mixtures. As part of internal dose assessment the radon and radon progeny concentrations are computed in a predefined dwelling, using advanced numerical calculation.

1 Experimental testing

1.1 Gamma-ray measurement

1.1.1 Principles of the method

The natural radioactivity concentrations are determined according to a standard method published under NEN 5697^[1]. According to this method the density dependent photo peak efficiencies are determined for the gamma-ray energies 352 keV (^{214}Pb), 583 keV (^{208}Tl), 911 keV (^{228}Ac) and 1,461 keV (^{40}K). Four calibration standards are assembled with increasing densities. The materials used are stearic acid, starch, gypsum and quartz sand, homogeneously mixed with certified amounts of ^{238}U and ^{232}Th , in equilibrium with their daughter nuclides, and ^{40}K . The standards are placed into Marinelli beakers with a volume of about 1 litre, weighted and closed radon-tight. To obtain secular equilibrium, a waiting time of at least three weeks is taken into account before counting the samples. All samples are counted using an HPGe detector in a low-background facility. The samples of the material are analysed in an identical way as the calibration standards with respect to geometry, waiting time and radon-tightness of the beaker. The photo-peak efficiencies of the samples are deduced from the efficiency curves of the standard samples by interpolation. The results are expressed per unit of dry weight.

1.1.2 Sample pre-treatment

The concrete samples are crushed and placed into a Marinelli beaker. To reach a secular equilibrium a waiting time of at least three weeks is applied before the samples are counted in an HPGe detector.

1.1.3 Results

Table 1 shows the results from the gamma-ray measurements. The counting time of each sample is 57,600 s. The standard deviation refers to the counting statistics.

Table 1 Sample specifications, activity concentration and standard deviation expressed in Bq/kg.

Sample code	Weight (kg)	Activity concentration (Bq/kg)							
		²²⁶ Ra		²²⁸ Th		²²⁸ Ra		⁴⁰ K	
		x	SD	x	SD	x	SD	x	SD
7013-A	1.443	34	2	6.1	0.5	6.0	0.4	48	3
7013-B	1.441	35	2	6.7	0.5	6.5	0.4	49	3
7013-C	1.523	35	4	5.8	0.6	5.8	0.5	46	2
7014-13	1.418	36	2	8.7	0.7	8.4	0.5	75	3
7014-14	1.544	33	3	8.5	0.8	7.9	0.8	68	5
7014-15	1.379	37	2	9.5	0.7	8.5	0.5	78	3
7015-13	1.474	36	4	9.9	0.9	10.2	0.7	48	2
7015-14	1.477	37	4	10.9	0.9	10.0	0.7	50	2
7015-15	1.512	37	2	10.9	0.7	9.8	0.5	49	3
7017-16	1.432	41	2	9.8	0.7	9.8	0.5	74	3
7017-17	1.505	40	2	8.3	0.6	8.8	0.5	73	3
7017-18	1.476	40	2	9.8	1.0	8.9	0.7	73	3
7019-20	1.544	36	2	9.2	0.6	9.3	0.5	55	3
7019-21	1.430	38	2	9.5	1.0	8.1	0.6	59	3
7019-22	1.148	47	4	10.9	1.0	11.3	0.8	72	3

1.2 Radon exhalation measurement

1.2.1 Principles of the method

The radon exhalation rate is determined according to the standard method NEN 5699^[2]. In this method the samples are enclosed in a container that is purged with nitrogen gas with a relative humidity of 50%. The three concrete prisms are placed in the container. The exhaled radon, carried along with the nitrogen gas, is trapped on silica gel at -190°C. After sufficient radon has been trapped, the nitrogen stream is stopped and the trapping agent analysed by liquid scintillation counting. The results are expressed as mass exhalation rates by normalizing the amount of exhaled radon per kg material.

1.2.2 Sample pre-treatment

The test samples for the ²²²Rn exhalation rate measurements are conditioned at a temperature of 20°C and a relative humidity of 50 %.

1.2.3 Results

The results from the radon exhalation measurements are given in Table 2. The standard deviation (SD) in this table refers to a triplicate analysis of the same test sample.

Table 2 Sample specifications and exhalation rate expressed as $\mu\text{Bq/s}$ and $\mu\text{Bq/kg/s}$.

Sample code	Exhalation rate					
	Weight (kg)	$\mu\text{Bq/s}$		$\mu\text{Bq/kg/s}$		(%)
		x	SD	x	SD	SD
7013	14.34	90.3	5.0	6.3	0.3	5.5
7014	14.40	87.2	19.8	6.1	1.4	22.6
7015	14.30	103.7	2.1	7.2	0.1	2.0
7017	14.42	84.4	15.9	5.9	1.1	18.9
7019	14.52	84.4	10.2	5.8	0.7	12.1

2 Radon simulation and boundary conditions

For the computation of the radon concentrations in the room a three dimensional numerical based software is used. For this purpose the details of the room are specified and the radon source for all five concrete mixtures is determined.

2.1 Geometry and boundary conditions

Based on information provided by the customer the following conditions of the room have been agreed:

Geometry and material features of the room

Dimensions	: length 3 m; width 3 m; height 2.7 m
Inner area	: 50.4 m ²
Volume	: 24.3 m ³
Window	: 1.2 x 1.2 m ² (1.4 m ²)
Door	: 2.0 x 0.8 m ² (1.6 m ²)
Area concrete	: 47.4 m ²
Concrete thickness	: 0.2 m
Concrete density	: 2300 kg·m ⁻³
Furniture	: Unfurnished room

Flow conditions and ²²²Rn background

Air exchange rate	: 0.5 h ⁻¹
²²² Rn background concentration	: 10 Bq·m ⁻³
²²² Rn background equilibrium factor	: 0.4

2.2 ²²²Rn source

In building materials the diffusion of ²²²Rn is often described as a one-dimensional process, i.e. directed to the living space and its opposite side. The ²²²Rn source for the considered room follows from the multiplication of the exhalation rates by the total area in the room taken by concrete and the surface density, the product of the thickness of the building parts and their density. In formula:

$$S = E_m A \rho L \quad (1)$$

In this equation S represents the ^{222}Rn source in the room ($\text{Bq}\cdot\text{s}^{-1}$); E_m the ^{222}Rn exhalation rate ($\text{Bq}\cdot\text{kg}^{-1}\cdot\text{s}^{-1}$); A the area in the room taken by concrete (m^2); ρ the density of concrete ($\text{kg}\cdot\text{m}^{-3}$); and L the half-thickness of the construction parts (m).

This method, however, has to be considered as a maximum. The exhalation from the test specimen takes place from all sides instead of one-dimensional as in a practical situation. This may lead to an overestimation of the ^{222}Rn source in the room under investigation. Berkvens et al.^[3] have introduced a formula to calculate the one-dimensional exhalation rate from the experimentally determined three-dimensional results. Therefore, they defined an equivalent sample geometry with a reduced thickness to compensate for the ^{222}Rn diffusion to the planes other than the front and backside. With the x-axis directed towards the room, the shortest mean distance is given by:

$$\frac{L'_x}{2} = \frac{L_x}{2} - \frac{1}{6} \left(\frac{L_x^2}{L_y} + \frac{L_x^2}{L_z} - \frac{1}{2} \frac{L_x^3}{L_y L_z} \right) \quad (2)$$

In this expression L_x , L_y and L_z represent half of the sample thickness of the test specimen in the x-, y- and z-direction. As the dimensions of the present test samples are $0.10 \times 0.10 \times 0.20 \text{ m}^3$, L'_x is calculated at 0.33 m. Subsequently the exhalation rate from a wall in practice is calculated from the measured exhalation rate according to:

$$\frac{E_m^{(1)}}{E_m} = \frac{L'_x \tanh(L_x/l)}{L_x \tanh(L'_x/l)} \quad (3)$$

$E_m^{(1)}$ in this equation is the one-dimensional exhalation rate; E_m the experimental determined exhalation rate; and l the diffusion length of ^{222}Rn in concrete. As reported by Kovler et al.^[4] the literature data on the diffusion length in concrete ranges from 0.06 m for heavy concretes to 0.30 m for light-weight species. If for the present concretes a diffusion coefficient of 0.10 m is assumed, a correction factor of 0.79 can be calculated from equation (3). With that the ^{222}Rn source for the five concrete mixtures is shown in the table below.

Table 3 Radon source in Bq/s for the five different concrete mixtures.

Sample code	Radon source (mBq·s ⁻¹)
7013	54
7014	52
7015	62
7017	50
7019	50

2.3 Radon and radon progeny modelling

The modelling of the ²²²Rn concentration and the concentrations of the short-lived ²²²Rn progeny nuclides ²¹⁸Po, ²¹⁴Pb and ²¹⁴Bi follows the method as described De With and De Jong^[5]. In this work, a Computational Fluid Dynamics (CFD) model is used to simulate the concentration of thoron and thoron progeny products in a typical Dutch living room. The dispersion is computed using the fundamental flow equations for gas and aerosols, which enables detailed simulation of the three-dimensional flow structures from ventilation and buoyancy. Extra algorithms are developed and coupled with the CFD model to take account of all relevant physical processes. These include the formation and attachment of the progeny products to aerosol particles as well as their dispersion and deposition.

The computed concentrations for radon and its progeny are as follows:

Table 4 Concentrations radon and radon progeny.

Sample code	²²² Rn (Bq·m ⁻³)	²¹⁸ Po (Bq·m ⁻³)	²¹⁴ Pb (Bq·m ⁻³)	²¹⁴ Bi (Bq·m ⁻³)
7013	26.1	22.2	9.5	4.9
7014	25.4	21.6	9.2	4.8
7015	28.5	24.2	10.3	5.3
7017	24.9	21.2	9.1	4.7
7019	24.8	21.2	9.1	4.7

These concentration levels also include the radon background concentration of 10 Bq·m⁻³ and its background progeny.

3 Dose assessment

3.1 Calculation of the external dose

The external dose due to gamma radiation from the building materials in the room is calculated according to the method described by De Jong et al.^[6,7]. The standard geometry as defined by Koblinger^[8] is taken as starting point for our calculation model. This geometry has dimensions of 5 x 4 m² and 2.8 m in height, with each construction part (i.e. floor, walls and ceiling) made of 20 cm thick concrete and no doors or windows. Correction factors have been deduced for alternative situations. The absorbed dose rate in air (unit: Gy·h⁻¹) in a particular room is then calculated according to:

$$\dot{D}_{air} = \left\{ \sum_{i=1}^6 [F_{dose} \cdot F_1 \cdot F_2 \cdot F_3 \cdot \dots \cdot F_n]_i \right\} F_{zoning} \cdot F_{adjac} \quad (5)$$

in which i is the index for a construction part, F_1 to F_n are the correction factors for construction part i , F_{zoning} is a correction factor which takes internal zoning of the construction into account, and F_{adjac} is the contribution from adjacent floors and dwellings. F_{dose} is the so-called dose factor, defined as:

$$F_{dose,i} = k_1 a_{1,i} + k_2 a_{2,i} + k_3 a_{3,i} \quad (6)$$

In this equation k_1 , k_2 and k_3 represent the specific absorbed dose rates, defined as the absorbed dose rate in air due to an activity concentration of 1 Bq·kg⁻¹ of each of the primordial radionuclides in equilibrium with its decay products (Gy·h⁻¹ per Bq·kg⁻¹); and $a_{1,i}$ to $a_{3,i}$ the activity concentration of ²²⁶Ra, ²³²Th and ⁴⁰K of construction part i (Bq·kg⁻¹), respectively. The values of the specific absorbed dose rate depend amongst others on the thickness, density and dimensions of the various construction parts.

Several researchers have determined the specific absorbed dose rate for the standard Koblinger-construction, using various codes. Averaged over all data the specific absorbed dose rates are^[9]:

²²⁶ Ra	0.90 nGy·h ⁻¹ per Bq·kg ⁻¹
²³² Th	1.10 nGy·h ⁻¹ per Bq·kg ⁻¹
⁴⁰ K	0.08 nGy·h ⁻¹ per Bq·kg ⁻¹

For the calculation of the annual indoor effective dose to the residents due to external radiation the absorbed dose as found from equation (5) is multiplied by a conversion factor of 0.7 Sv·Gy⁻¹ and the

annual number of hours spent indoors, taken as 7000. The mean activity concentrations for the five concrete mixtures are as follows:

Table 5 Activity concentrations.

Sample code	²²⁶ Ra (Bq·kg ⁻¹)	²³² Th (Bq·kg ⁻¹)	⁴⁰ K (Bq·kg ⁻¹)
7013	35	6	48
7014	35	9	74
7015	37	10	49
7017	40	9	73
7019	40	10	62

Based on those experimental results the annual external dose for is as follows:

Table 6 Annual external dose from primordial radionuclides.

Sample code	External dose (mSv·a ⁻¹)
7013	0.20
7014	0.23
7015	0.24
7017	0.26
7019	0.25

3.2 Calculation of the internal dose

The effective dose to residents due to inhalation of the short-lived ²²²Rn progeny is based on the so-called equilibrium equivalent ²²²Rn concentration. This concentration is calculated according to the following expression:

$$C_{eq}^{222} = 0.105 C_1 + 0.515 C_2 + 0.380 C_3 \quad (4)$$

in which C_1 , C_2 and C_3 are the activity concentrations in the indoor environment of ²¹⁸Po, ²¹⁴Pb and ²¹⁴Bi (Bq·m⁻³), respectively, as found by the model computations. The constants in the equation are the relative contributions of each decay product to the total potential alpha energy from the decay of a unit ²²²Rn gas. To convert the equilibrium equivalent concentration into an effective dose rate, a conversion factor of 9 nSv·h⁻¹ per Bq·m⁻³ is applied^[10]. The time spent indoors is taken as 7000 h per year (80% of the total time).

Based on the findings reported in Table 4, the above conversion factor and the hours spent indoors the internal dose is as follows:

Table 7 Annual internal dose from radon exposure.

Sample code	Internal dose (mSv·a ⁻¹)
7013	0.57
7014	0.56
7015	0.62
7017	0.55
7019	0.55

3.3 Calculation of the total dose

Based on the calculated internal and external dose as presented in Table 6 and Table 7 the total annual dose is:

Table 8 Annual total dose from primordial radionuclides.

Sample code	Total dose (mSv·a ⁻¹)
7013	0.78
7014	0.79
7015	0.86
7017	0.80
7019	0.80

4 Conclusions

The findings of this work are as follows:

1. The activity concentrations and radon exhalation have been experimentally investigated for five different concrete mixtures.
2. The results indicate that the ^{226}Ra concentration is between 35 and 40 $\text{Bq}\cdot\text{kg}^{-1}$, and broadly similar for all concrete mixtures. The ^{228}Th and ^{228}Ra concentration varies between 6 and 11 $\text{Bq}\cdot\text{kg}^{-1}$, while the concentration ^{40}K varies between 48 and 75 $\text{Bq}\cdot\text{kg}^{-1}$.
3. The radon exhalation varies between 5.8 and 7.2 $\mu\text{Bq}\cdot\text{s}^{-1}\cdot\text{kg}^{-1}$.
4. Based on computational modelling the radon concentration for a room of $3\times 3\times 2.7\text{ m}^3$ and an air exchange rate of 0.5 h^{-1} is estimated between 25 and 29 $\text{Bq}\cdot\text{m}^{-3}$. This includes a background concentration of $10\text{ Bq}\cdot\text{m}^{-3}$.
5. Computation of the external and internal dose for those concrete mixtures results in an estimated yearly external dose of up to 0.26 mSv and an internal dose of up to 0.62 mSv.

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